SCRIPPS REFERENCE GAS CALIBRATING SYSTEM FOR CARBON DIOXIDE IN AIR STANDARDS: REVISION OF 1981

A REPORT PREPARED FOR THE ENVIRONMENTAL MONITORING PROGRAM OF THE WORLD METEOROLOGICAL ORGANIZATION

by

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Introduction

This report describes the system of carbon dioxide in air $(CO_2-in-air)$ gas standards developed at the Scripps Institution of Oceanography. These gas mixtures are for the purpose of determining the corrections needed when air is compared with gas standards containing carbon dioxide in nitrogen (CO_2-in-N_2) using the nondispersive infrared gas analyzer installed at the Scripps Laboratory since 1956.

This is the second in a series of reports describing the reference gas standards developed by the Scripps Institution of Oceanography. An earlier report entitled "CO₂ Reference Gas System" [Bacastow et al., 1983] describes the system of CO_2 -in-N₂ gas standards. It should be referred to for nomenclature and description of the Scripps Reference Gas System.

When CO_2 -in-N₂ gases are employed to measure CO_2 -in-air with the Scripps Applied Physics Corporation (APC) infrared analyzer installed at Scripps Laboratory, a correction of approximately 4 ppm must be made because of the difference in line broadening introduced by replacing 20.9% of the nitrogen by oxygen and 0.9% of the nitrogen by argon [Keeling et al., 1976; Griffith et al., 1982]. An additional correction of approximately 0.4 ppm must be made if the APC analyser is operated at lower ambient pressure, such as exists at Mauna Loa Observatory, Hawaii and the South Pole, where similar laboratory analyzers are or have been operated. A new determination of these corrections, made in connection with the 1981 calibration of the reference gas system, is described herein.

Manometric Air Standards

During 1980 and 1981, a suite of 12 cylinders were specially cleaned and then were filled with dry, filtered air at the Scripps Diving Locker. A Rix water lubricated piston compressor pump was used, and the air was pumped only during days when it was especially free of pollution. These gas mixtures are designated primary manometric standards for the Scripps CO_2 -in-air reference gas system. They are stored in "white stripe" cylinders.

Before filling, the cylinders (standard 250 cubic foot chromemolybedium steel tubes) were sent out to a commercial gas supply firm to be cleaned inside by a process that involves (1) tumbling with carborundum grit, (2) steam cleaning, and (3) etching with muriatic acid. There is some doubt that all of these procedures were actually carried out, but, in any case, all cylinders were probably treated in the same way. After the cylinders were returned to Scripps and filled, the air was rejected if it contained more than 10 ppm water vapor, as measured by a U.S. Bureau of Mines type dew point tester, and a new filling made. Those CO_2 gas mixtures retained after moisture testing were adjusted to the desired concentrations by removing CO_2 with ascarite or by adding reagent grade CO_2 gas (Airco grade 4).

These cylinders were manometrically analyzed, mostly in 1981, and their nitrous oxide (N_20) concentration determined by Dr. Ray Weiss, of the Scripps Institution of Oceanography. The trace gas, N_20 , is included with CO_2 in the manometric analysis, so a correction of approximately 0.30 ppm was made for it to each cylinder. The N_20 data were obtained using a gas chromatograph with a flame ionization detector. The manometric data are listed in Tables Ia to 1d including, for completeness, measurements made in 1974 and of artificial as well as natural air. The manometric concentrations corrected for N_20 , are listed in Table 2a and 2b.

Infrared Analyzer Calibrations

Using the APC analyzer these 12 CO_2 -in-air cylinders were compared by infrared analysis to the Principal Span and High Span CO_2 -in-nitrogen reference gases of the Scripps reference gas system during five days between 18 August and 1 September, 1981 (Table 3a). The 12 manometric values, corrected for N₂O, have been fit to the obtained adjusted index values, J81, by a cubic relation:

$$X = CUB9(J81)$$

(1)

 $= 86.984 + 0.523638(J81) + 5.0398x10^{-4}(J81)^{2} + 5.5214x10^{-7}(J81)^{3}$

- 3 -

where J81, refers to adjusted index values obtained at the time of the 1981 calibration.

Together with the 1980 calibration of $\text{CO}_2-\text{in-N}_2$ manometric standards, this calibration would provide all the information needed to establish a line broadening correction at standard atmospheric pressure, were it not for the problem of system drift in the $\text{CO}_2-\text{in-N}_2$ standards.

Drift of the CO2-in-N2 System between 1980 and 1981 Calibrations

Cylinders of CO_2 -in-N₂ or CO_2 -in-air may change in concentration with time for reasons that are thought to be related to surface interactions in the cylinder, fractionation effects associated with flow through the valves, or slow introduction of laboratory air into the cylinders at times of pressure regulator installations. In most cases, the compositions of Scripps primary standards when determined directly by a manometric technique have been found, however, to be reasonably stable.

Thus the drift is in the "system"; it involves changes with time of the relation between true concentration (X) and the Adjusted Index value (J), found by comparison to the reference gas system Principal and High Span standards to manometric standards. There is evidence that it is related to the procedure of determining new Principal and High Span standards by comparison to older Principal and High Span standards such that very small changes in concentration for individual standards yield a cumulative affect on the overlapping system [Bacastow et al., 1983]. In order to apply the 1981 CO_2 -in-air calibration data generally, it is first necessary to correct J values for system drift relative to the 1980 CO_2 -in-N₂ calibration, to which the CO_2 -in-N₂ data are first adjusted.

Information to determine this system drift between 1980 and 1981 was obtained by infrared comparisons of four of the $\text{CO}_2-\text{in-N}_2$ manometric standards, made in conjunction with comparisons of five of the 12 CO_2 -in-air primary manometric standards, near the time of the calibration of the 12 CO_2 -in-air standards in 1981, as described above (Table 3b). These $\text{CO}_2-\text{in-N}_2$ standards have been shown to be stable between 1974 and

1980 [Bacastow et al., 1983]. The drift, J81 - J80, is summarized in Table 4 and a quadratic fit, shown in Figure 1, was found, as follows:

J81 - J80 = OUAD10(J80)

$$= -1.952 + 0.013966(J80) - 2.5281 \times 10^{-3} (J80)^2$$
(2)

For times of infrared analysis between the 1980 and 1981 calibrations, we use linear interpolation to determine J80 from the observed value, J:

$$J = J80 + (D - CD80) / (CD81 - CD80) OUAD10(J80)$$
(3)

where CD81 denotes the central date for the 1981 calibration, 9 September 1981. The above equation is solved for J80 by iteration. For times before CD80, the central date of the 1980 calibration, we employ the drift correction described by Bacastow et al. [1983] to calculate J80. Afterwards all data, before or after CD80, are adjusted to J81 via Equation (2).

1981 Air Calculation

This is obtained by calculating the mole fraction X via Equation (1) from the J8l adjusted index values, calculated as just described. The reproducibility of equation (1) is illustrated by its goodness of fit to the 12 CO_2 -in-air gas mixtures as shown in Table 5.

1974 WMO Air Correction

The 1974 WMO Scale air correction is represented as a factor with which the observed adjusted index value (J) is multiplied before using the cubic curve relating concentration (X) to analyzer response (J) for CO_2 -in-N₂ gases. Specifically, for CO_2 -in-air gases measured relative to CO_2 -in-N₂ standards, Keeling et al. [1976] have reported the equation

$$X = CUBW(10(1.01201J))$$

(4)

- 5 -

where CUBWMO is the originally determined $1974 \text{ CO}_2 - \text{in-N}_2$ calibration curve:

$$CUBW10(J) = 76.582 + 0.584910(J) + 3.1151 \times 10^{-4} (J)^{2}$$

 $+ 7.335 \times 10^{-7} (J)^3$

Equation (5) is essentially the same as

$$X = CUB1(1.01201J)$$
(6)

(5)

where CUB1 is the CO_2 -in-N₂ calibration curve for 1974 associated with the 1980 calibration:

$$CUB1(J) = 77.455 + 0.573302(J) + 3.5735x10^{-4}(J)^{2} + 6.7618x10^{-7}(J)^{3}$$
(7)

CUBI differs from CUBWMO only in that it is based on more manometric measurements of the CO_2 -in- N_2 standards. Thus the air correction in current use, for J obtained any time during the project, is equivalent to:

$$\underline{/J} = 0.01201 J \tag{8}$$

Comparison of the 1981 Air Correction with Additional Data

Table 5a and Figures 2 and 3 show a representation of the 1981 air correction in the same form as the 1974 air correction. Figure 2 displays only data from the 12 manometric CO_2 -in-air standards described above. Figure 3 displays these data (as circles) plus additional data:

- [1] Measurements (shown as plus marks) of five of the twelve CO_2 -in-air manometric standards on the five days when four of the CO_2 -in- N_2 standards were run to obtain data for the J81-J80 drift correction (Table 6b).
- [2] Measurements (shown as crosses) of three air surveillance standards near the time of the 1980 CO_2 -in-N₂ calibration (Table 6c).
- [3] Measurements (shown as squares) of the three surveillance standards mentioned in [2] above, plus two others, near the time of the 1974 calibration (Table 6d). These are the data that led to the 1974 WMO Air Correction.

It is apparent from Figure 3 that the 1974 air measurements are about (0.0004)(330) = 0.13 ppm higher at 330 ppm than the 1980 air measurements.

Source Block Correction

On October 30, 1980, the ascarite trap on the source block was observed to be exhausted and ineffective. The trap is intended to remove CO_2 and water vapor from air in the source optical path where the infrared beam is split, part going through the reference cell and part through the sample cell. At this location, CO_2 might be expected to effect line broadening and, consequently, the air correction.

The trap is not easily accessed for ascarite replacement. Discussions with personnel responsible for the maintenance of the analyzer indicate that the ascarite in 1980 probably had not been replaced for the last six years.

An examination of data for CO₂-in-air surveillance standards (see Table 7) supports a small correction before October 30, 1980, raising J values approximately 0.11 ppm near air concentration. This correction would approximately bring the 1974 air correction data, depicted by squares in Figure 3, into accordance with the 1981 data. (Higher J values after correction result in a smaller carrier gas correction.) Since the air correction, as indicated in Figure 3, is approximately proportional to J, the offset prior to October 30, 1980, has been represented by

$$//J = 0.00033(J)$$
 (9)

Pressure Correction to the Air Correction as Determined in 1974

A pressure broadening correction would be expected to vary with total pressure in the gas analyzer sample chamber, and indeed this has been found to be the case. Keeling et al. [1976] report a correction equivalent to

$$\frac{\Lambda J}{J} = 0.003157 - 2.237 \times 10^{-6} (P) - 2.522 \times 10^{-9} (P)^2$$
(10)

where P is the chamber pressure in mmHg. At the average Mauna Loa Observatory station pressure of 509.9 mm, the correction is //J/J = 0.00136. For a J value of 330 ppm, the correction is thus 0.45 ppm.

1981 Pressure Correction to the Air Correction

In 1981 more extensive data were obtained at two reduced pressures for CO_2 -in-air and CO_2 -in-N₂-and-O₂ standards (Table 8). The cell pressure was controlled with a cartesian diver manostat, as done for the 1974 data.

A simple equation has been fit to the 1981 data:

$$\Delta J = a_1 J(\Delta P)C(1 + a_2 \Delta P)(1 + a_3 C)$$
(11)

where the a_i are coefficients to be determined by the fits, ΔP is the difference in pressure in mmHg from 760.46 mmHg, and

 $C = (\%0_{2}) + 1.5(\%A)$ (12)

The factor of 1.5 in the above equation derives from information in Tables 10 and 11 of Guenther and Keeling [1981]. The correction for argon is approximately 0.26 ppm; its "effectiveness" relative to oxygen is thus approximately

$$\frac{0.26/0.93}{3.9/20.9} \sim 1.5 \tag{13}$$

The fit (Table 9) is quite good. Values of the fitted coefficients are

$$a_1 = (1.51 \pm 0.15) \times 10^{-7}$$

 $a_2 = (9.48 \pm 2.51) \times 10^{-4}$
 $a_3 = (8.01 \pm 6.48) \times 10^{-4}$

Clearly, a_3 is not significant and could have been omitted from the computation. The pressure correction at the average Mauna Loa Observatory pressure (509.9 monthly) is then //J/J = 0.00107, or 0.35 ppm at 330 ppm.

The 0.10 difference between pressure corrections as found from 1974 and 1981 data is probably a result of more and better data in 1981.

Comparison with NBS Standards

During June of 1980 Dr. Ernest Hughes of the U.S. National Bureau of Standards visited the Scripps $\rm CO_2$ Laboratory. He brought with him three cylinders of $\rm CO_2$ -in-air gas mixtures which had been compared by infrared and gas chromatographic analysis against primary gravimetric standards. The latter had been synthesized by a gravimetric procedure to be described in an article in preparation. Each gas mixture was analyzed twice by Peter Guenther at Scripps in the same manner as the other gas mixtures reported in Tables 1a - 1d. The results are listed in Table 1C. The contents of $\rm N_2O$, analyzed in the laboratory of Dr. Ray Weiss, are listed in Table 2b, together with corrected $\rm CO_2$ mole fractions. The agreement between the Scripps and NBS results is very close, as indicated by the comparisons listed in Table 10. On average the NBS mixtures were 0.09 ppm higher than the Scripps results. The standard deviation in the mean of the differences was 0.05 ppm.

Acknowledgements

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tric	analyses	of	CO ₂ -in-air	standards	; (
		Tra	liniduo 1	Dur	0

			Individual	Run	Overall	
Cylinder	Run		Determinations	Average	Average	No. of
No.	No.	Date	(ppm)	(ppm)	<u>(ppm)</u>	Runs
	÷ .					
35435	1	22 JAN 74	334.42	334.38	334.40	3
	2	23 JAN 74	334.46	334.48		,
	3	7 MAR 74	334.29	334.33		
35405	1	10 APR 74	337.29	337.26	337.28	2
	2	11 APR 74	337.27	337.30		
34770	1	10 MAY 74	338.67	338.77	338.84	2
	2	15 MAY 74	338.90	338.90		
35401	Run	Number 1 Con	taminated			
	2	10 MAY 74	353.26	353.25	353.26	2
	3	15 MAY 74	353.21	353.28		
35378	1	7 MAY 74	355.82	355.88	355.93	2
	2	8 MAY 74	355.98	355.98		

during 1974. Table la. Manome

Table 1b. Manometric analyses of CO_2 -in-nitrogen-and-oxygen standards during 1974.

Cylinder	Run		Individual Determinations	Run Average	Overall Average	No. of
No.	No.	Date	(ppm)	(ppm)	(ppm)	Runs
44726	1	10 APR 74	¥ 309.48	309.56	309.57	2
			309.64			
	2	12 APR 74	309.59	309.58		
0.5 / 5 -			309.58			
35452	1	13 FEB 74	323.82	323.80	323.86	2
			323.85			
			323.74	s. 1		
			323.77	•.		
	2	14 FEB 74	323.86	323.91		
			323.91			
25/2/	-		323.95			
35434	T	26 FEB 74	323.97	323.96	323.91	2
			323.99			
	0		323.92			
	2	27 FEB 74	323.87	323.86		
25440	-		323.85			
35442	T	5 MAR 74	326.96	327.02	327.02	2
	•	-	327.09			
	2	/ MAR 74	326.97	327.01		
25//1	-	/	327.05			
35441	T	1 MAR 74	331.99	331.98	332.04	2
	0		331.96			
	2	I MAR /4	332.12	332.10		
25200	-	07 777 74	332.08			
35389	T	27 FEB 74	335.21	335.30	335.36	2
			335.38			
	2	28 FEB /4	335.31	335.41		
11605	-	10 +== =/	335.51			
44095	T	12 APR 74	351.98	352.00	351.92	2
	•	1	352.01	_		
	2	15 APR 74	351.75	351.84		
			351.94			

Table 1c. Manometric analysis of CO₂-in-air standards during 1980-1981.

				Individual	Run	0verall	
Cylinder	Run			Determinations	Average	Average	No. of
NO.	NO.	Date		(ppm)	<u>(ppm)</u>	<u>(ppm)</u>	<u>_Runs</u>
66556	7	18 TUN	80	101 40	101 30	101 36	2
00000	Ŧ	TO 20M	00	101 38	101.39	TOT • 20	Z
	2	6 AUG	81	101.30	101 33		•
	-	0 1100	01	101.35	101.33		
71251	1	18 JUN	80	213.54	213 52	213 49	2
	-	10 000		213.50	210.02	213.47	-
	2	6 AUG	81	213.48	213.46		
				213.43			
34819	1	7 AUG	81	251.95	251.92	251.96	2
				251.90			
-	2	12 AUG	81	251.99	252.00		
				252.01	· ·		
71286	1	24 OCT	80	296.88	296.90	296.88	2
				296.91			
				296.91			
	2	7 AUG	81	296.88	296.86		
				296.85			
71341	1	12 AUG	81	322.72	322.70	322.76	2
				322.69			
	2	13 AUG	81	322.82	322.82		
				322.83			
<u>66638</u>	1	13 AUG	81	338.45	338.44	338.39	2
				338.43			
	2	14 AUG	81	338.35	338.34		
				338.32		· _	
66625	1	14 AUG	81	344.90	344.86	344.91	2
	_			344.82			
	2	18 AUG	81	344.96	344.96		
66696	1	18 AUG	81	360.17	360.15	360.18	2
		10		360.13			
	2	19 AUG	81	360.21	360.22		
71200	-	0.6 1.170	0 1	360.22	074 04	074 00	-
/1308	Τ	26 AUG	81	3/6.8/	3/6.84	3/6.80	2
	0	07 410	0.1	3/6.81	076 76		
	2	Z/ AUG	δT	3/0.//	3/6./6		
				3/0./0 276 7/			
\$				3/0./4 376 75			
				3/0./3			

Table 1c (Cont.).

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s.

				Individual	Run	Overal1	
Cvlinder	Run			Determinations	Average	Average	No. of
No.	No.	Date		(ppm)	(ppm)	(ppm)	Runs
71370	1	25 AUG	81	406.66	406.66	406.70	2
113/0	-		•	406.67			
	2	26 AUG	81	406.75	406.74		
				406.72	•		
71479	1	24 AUG	81	453.73	453.72	453.70	2
				453.72	. · · ·		
	2	24 AUG	81	453.69	453.68		
				453.66			0
67615	1	20 AUG	81	503.38	503.39	503.50	2
				503.40			
	2	20 AUG	81	503.63	503.62		
	-	16 36437	0.0	503.61	227 22	227 27	n
35405	Ŧ	16 MAY	80	33/.32 227 22	337.32	551.21	4
	2	22 MAV	20	337 26	337 22		
	2	25 MAI	80	337 10	JJ7 • 22		
3/770	. 1	15 MAV	ឧក	339 12	339.12		
34770	T	T) NU	00	339.13	557.12		
	2	16 MAY	80	339.53	339.52		
	-		00	339.50			
	3	29 MAY	80	338,75	338.75	338.71	. 2*
	•			338,75	•	· ·	
	4	13 JUN	80	338.67	338.67		
				338.67			
35401	1	30 MAY	80	353.03	353.00	353.02	3
				352.97			
	2	30 MAY	80	353.07	353.05		
				353.03			
	3	5 AUG	81	353.02	353.02		
				353.03			
NBS Cylind	ers						
		2 TITN	80	333 56	333,54	333,50	2
62206	T	אַטע כ	00	333 51	555.51		
	2	/ TIM	80	333.49	333.47		
	2	4 001	00	333.45			
61120	1	4 TIN	80	340.26	340.25	340.22	2
01120	-	- 000	00	340.24	-		
	2	10 JUN	80	340.22	340.18		
	-		·	340.15			
243988	1	30 MAY	80	347.00	346.96	346.97	2
2,0,00				346.91			
	2	9 JUN	80	346,96	346.98		
				347.01			

* Runs 1 and 2 deleted due to instrumental problems

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				Individual	Run	Overal1	
Cylinder No.	Run No.	Date		Determinations (ppm)	Average (ppm)	Average (ppm)	No. of Runs
75934	1	5 JUN 8	80	338.29	338.27		
				338.25			
	2	10 SEP 8	80	339.10	339.08	339.04	2*
			•	339.05			
	3	11 SEP 8	80	338.99	339.00		
			_	339.01			÷
127524	1	13 JUN 8	80	339.58	339.64		
			• •	339.72			0.4
	2	9 SEP 8	80	340.28	340.30	340.38	2*
	-		• •	340.32	010 15		
	3	16 SEP 8	80	340.42	340.45		
	-		• •	340.48	0.61 01		
127693	1	16 JUN 8	80	360.98	361.04		
	_		~ ~	361.11	0.61 //	267 10	0.4
	2	9 SEP a	80	361.41	361.44	361.48	2*
	•	17	~ ~	361.46	261 50		
	3	1/ SEP 3	80	361.54	361.52		
	-	-	~~	361.50	202 ((222 66	2
35452	L.	II NOV 8	80	323.65	323.00	323.00	Z
	0	10 1007	~~	323.68	202 (5		
	2	12 NOV 8	80	323.66	323.05		
0 = / / 1	-	10 1007	~~	323.64	221 01	221 00	2
35441	T	L3 NOV 8	80	331.94	331.91	331.90	. 2
		12 101	00	JJL.88	221 00		
	2	13 NOV 6	80	JJL.00 221 07	221.00	·	
25//2	-	1/ 1011	00	JJL.0/	226 80	226 01	r
35442	T	14 NOV 6	00	226.70	320.00	J20.01	2
	2	14 NOV	00	220.19	376 82		
	Z	14 NOV	00	320.03	320.02		
25290	1	19 1017	00	320.02	225 52	335 /8	2
33309	Ŧ	TO NON O	00	335 50	22.00	555.40	<u>ک</u>
	n	10 NOV	<u>_</u>	335 /5	335 44		
	2	IJ NOV (00	335 43	555.44		
25/2/	1	10 NOV	00	322.80	322 70		
55454	Т	IS NOV	00	322.00	522.19		
	2	20 NOV	80	373 87	373 87	323 80	2+
	2	20 NOV 0	00	323.02	J_J.02	J_J,00	- 1 -
	2	21 NOT	80	323 80	323 70		
	J	21 NOV 0	00	323.00	565.13		
				363410			

Table 1d. Manometric analyses of CO₂-in-nitrogen-and-oxygen standards during 1980.

*Run No. 1 deleted because of apparent drift in tank concentration †Run No. 1 deleted because it is not consistent with other two Table 2a. N₂O corrected concentration of CO₂-in-air standards manometrically analyzed during 1974.

	Cylinder No.	Manometric Average* (ppm)	N ₂ O Concentration (ppm)	Corrected Concentration (ppm)
Red	Stripe Cylinders			
	35435	334.40	0.29	334.11
	35405	337.28	0.29	336.99
	34770	338.84	0.29	338.55
	35401	353.26	0.30	352.96
	35378	355.93	0.29	355.64
			· · · · · · · · · · · · · · · · · · ·	

*See Table la

Table 2b. N_2^0 corrected concentration of CO_2^- in-air

standards manometrically analyzed during 1980-81.

	Cylinder No.	Manometric Average* (ppm)	N ₂ O Concentration (ppm)	Corrected Concentration (ppm)
Whi	ite Stripe Cvi	linders		
	66556	101.36	0.37	100.99
	71251	213.49	0.34	213.15
	34819	251.96	0.24	251.72
- 1	71286	296.88	0.32	296.56
	71341	322,76	0.31	322.45
	66638	338.39	0.31	338.08
	66625	344.91	0.29	344.62
	66696	360.18	0.31	359.87
	71308	376.80	0.32	376.48
	71370	406.70	0.31	406.39
	71479	453.70	0.30	453.40
	67615	503.50	0.30	503.20
Red	l Stripe Cylir	$ders^{\dagger}$	ţ	
	35405	337.27	0.29	336.98
	34770	338.71	0.29	338.42
	35401	353.02	0.30	352.72
NBS	Cylinders			
	62206	333.50	0.30	333.20
	61130	340.22	0.31	339.91
	243988	346.97	0.29	346.68

* See Table lc

 $^{+}N_{2}^{0}$ values same as in Table 2a

Table 3a. Applied Physics infrared analyzer results from comparison to Scripps System CO_2 -in-nitrogen standards for 12 manometrically analyzed CO_2 -in-air standards during 1981 calibration. The entries, in ppm, are Index (I), except for the last column, which is Adjusted Index (J). The numbers in parentheses indicate the number of comparisons.

Cylinder No.	18 AUG	20 AUG	25 AUG	27 AUG	<u>1 SEP</u>	Average	<u> </u>
66556	77.20(10)	77.82(20)	77.15(12)	77.55(10)	76.18(10)	77.18	25.96
71251	216.61(10)	217.20(10)	216.50(10)	216.91(10)	216.25(10)	216.69	195.96
34819	255.14(10)	255.43(10)	255.11(10)	255.23(10)	254.95(10)	255,17	242.85
71286	295.47(10)	295.58(10)	295.51(10)	295.52(10)	295.39(10)	295.49	291.99
71341	316.90(10)	316.94(10)	316.98(10)	316.97(10)	316.85(10)	316.93	318.12
66638	329.65(10)	329.49(10)	329.50(10)	329.60(10)	329.56(10)	329.56	333.51
66625	334.58(12)	334.59(12)	334.63(10)	334.54(10)	334.63(10)	334.59	339.64
66696	346.24(10)	346.31(10)	346.32(10)	346.33(10)	346.30(10)	346.30	353.91
71308	358.46(10)	358.56(12)	358.59(10)	358.61(10)	358.54(12)	358.55	368.83
71370	379.82(10)	379.90(10)	379.96(10)	380.00(10)	379.93(10)	379.92	394.87
71479	411.36(10)	411.63(10)	411.51(10)	411.64(10)	411.33(10)	411.49	433.35
67615	442.20(10)	442.66(10)	442.41(10)	442.64(10)	442.26(10)	442.43	471.05

Table 3b. Applied Physics infrared analyzer results for 4 CO₂-in-nitrogen standards and 5 CO₂-in-air standards from comparison to Scripps System CO₂-in-nitrogen standards during time close to 1981 calibration. The entries, in ppm, are Index (I), except for the last column, which is Adjusted Index (J). The numbers in parentheses indicate the number of comparisons.

Cylinder						Average	
No.	31 AUG	<u>3 SEP</u>	8 SEP	<u>10 SEP</u>	<u>14 SEP</u>	<u> </u>	$\overline{\mathbf{J}}$
CO2-in-nitrog	gen Standards						
2408	201.02(10)	200.95(10)	200.57(12)	200,96(10)	200.84(10)	200.87	176.68
7366	280.66(10)	280.70(10)	280.53(10)	280.70(10)	280.62(14)	280.64	273.89
39239	328.34(10)	328.39(10)	328.41(10)	328.44(10)	328.34(10)	328.38	332.07
35316	427.81(10)	427.81(10)	427.72(10)	427.87(10)	427.70(10)	427.78	453.20
CO ₂ -in-air St	tandards						
71251	216.64(10)	216.69(10)	216.28(10)	216.75(10)	216.44(10)	216.56	195.80
71286	295.41(10)	295.54(10)	295.41(10)	295.53(10)	295.45(10)	295.47	291.96
66638	329.58(10)	329.53(10)	329.54(10)	329.60(10)	329.56(10)	329.56	333.51
71370	379.89(10)	379.92(10)	379.84(10)	379.89(10)	379.78(10	379.86	394.80
67615	442.28(10)	442.33(10)	442.17(10)	442.33(12)	442.14(10)	442.25	470.83

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Table 4. Data summary of 1981 correction for CO₂-in-nitrogen Reference Gas System drift between the central dates, CD80 and CD81. Adjusted index values (in ppm) in columns headed J80 and J81 are from special calibrations in 1980 [see Bacastow et al., 1983, Table 3] and 1981 (Table 3b), respectively.

Cylinder No.	<u>J80</u>	<u>J81</u>	<u> J81–J80</u>
CO2-in-nitrog	en Standards		
2408	176.96	176.67*	-0.29
7366	273.84	273.89	0.05
39239	332.24	332.07	-0.17
35316	454.01	453.20	-0.81

"Error detected in final proofing of report. See Table 3b. (Correct value, .01 ppm higher, is not shown and is not used in curve fits.) Table 5. Summary of CO_2 -in-air standards calibration relative to Scripps System CO_2 -in-nitrogen standards. The column headed "Residual" is measured concentration less calculated concentration. The fitted equation is given in the text (Eq. (1)).

Concentration X (ppm)	Adjusted Index J (ppm)	Residual (ppm)
linders	the second s	
100.99	26.08	0.00
213.15	195.96	0.05
251.72	242.85	-0.06
296.56	291.99	-0.03
322.45	318.12	0.11
338.08	333.51	-0.08
344.62	339.64	0.02
359.87	353.97*	-0.10
376.48	368.83	0.10
406.39	394.87	0.06
453.40	433.35	-0.08
503.20	471.05	0.02
	Concentration X (ppm) vlinders 100.99 213.15 251.72 296.56 322.45 338.08 344.62 359.87 376.48 406.39 453.40 503.20	Concentration Adjusted Index X J (ppm) (ppm) vlinders 100.99 26.08 213.15 195.96 251.72 296.56 291.99 322.45 338.08 333.51 344.62 359.87 353.97* 376.48 406.39 394.87 453.40 433.35 503.20 471.05

* Error detected in final proofing of report. See Table 3a. (Correct value, .06 ppm lower, is not shown and not used in curve fits.) Table 6a. Comparison of 1981 CO₂-in-air calibration and 1980 CO₂-in-nitrogen calibration expressed in adjusted index, J, and mole fraction, X (both in ppm). The columns headed by "Points" and "Curve" refer to data plotted in Figures 2 and 3. The column labeled J81X is obtained by inverting CUB9(J), the CO₂-in-air curve (see Table 5). The column labeled J80X' is similarly obtained by inverting CUB2(J), the 1980 CO_2 -in-nitrogen curve (the prime indicates that although the gas is CO_2 -in-air we have used the CO_2 -in-nitrogen curve). The column labeled J81X' is obtained by correcting J80X' for the system drift between 1980 and 1981 calibrations by use of QUAD10 (see Figure 1). All data are as obtained during the days in which all 12 CO_2 -in-air standards were compared with Scripps System CO_2 -in-nitrogen standards (see Table 3a).

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	Mea	asured		Calculat	ed	Points	3	Curv	e
Cylinder No.	J81	<u>x</u>	J81X	J80X'	J81X'	∆J = p J81X'-J81	∆J_/J81X	$\Delta J_{c} = J81X' - J81X$	∆J _c /J81X
66556	26.08	100.99	26.08	29.92	28.36	2.28	0.08742	2.28	0.08742
71251	195.96	213.15	196.02	198.35	198.17	2.21	0.01127	2.15	0.01097
34819	242.85	251.72	242.78	245.55	245.50	2.65	0.01092	2.72	0.01120
71286	291.99	296.56	291.95	295.34	295.31	3.32	0.01137	3.36	0.01151
71341	318.12	322.45	318.23	321.99	321.91	3.79	0.01191	3.68	0.01156
66638	333.51	338.08	333.43	337.42	337.30	3.79	0.01137	3.87	0.01161
66625	339.64	344.62	339.66	343.74	343.60	3.96	0.01166	3.94	0.01160
66696	353.97	359.87	353.88	358.17	357.98	4.01	0.01133	4.10	0.01159
71308	368.83	376.48	368.92	373,44	373.18	4.35	0.01179	4.26	0.01155
71370	394.87	406.39	394.92	399.83	399.42	4.55	0.01152	4.50	0.01140
71479	433.35	453.40	433.29	438.76	438.07	4.72	0.01089	4.78	0.01103
67615	471.05	503.20	471.06	477.06	476.02	4.97	0.01055	4.96	0.01053

Table 6b. Comparison of the 1980-81 air correction with measurements obtained for CO_2 -in-air standards on days when CO_2 -in-nitrogen primary standards were compared to give the J81-J80 correction (Table 3b, Figure 1). The nomenclature is as in Table 6a.

	Measu	red		Calculated	-		
Cylinder No.	J81	<u>x</u> . —	J81X	J80X'	J81X'	$\Delta J_{p} = J81X' - J81$	∆J_/J81
	. •					• • • • • • • •	
71251	195.80	213.15	196.02	198.35	198.17	2.37	0.01209
71286	291.96	296.56	291.95	295.34	295.31	3.35	0.01148
66638	333.51	338.08	333.43	337.42	337.30	3.79	0.01137
71370	394.80	406.39	394.92	399.83	399.42	4.62	0.01170
67615	470.83	503.20	471.06	477.07	476.02	5.19	0.01102

Table 6c. Comparison of the 1980-81 air correction with measurements of CO_2 -in-air gas mixtures measured near the central date of the 1980 CO_2 -in-nitrogen calibration. Manometric measurements, X, are from Table 1c. Nomenclature is as in Table 6a.

Cylinder	4				Calculat	ted		∆J_ =	
No.	$\mathbf{J80}^{T}$	Х		J81X	J80X'	J81X'	J81	J81X ⁹ -J81	∆J_/J81
		_		Star and Star Street Street		State of Sta			<u>p</u>
									•
35405	332.29	336.9	8	332.38	336.35	5 336.23	332.19	4.04	0.01215
34770	333.84*	338.4	2	333.76	337.75	5 337.63	333.73	3.90	0.01168
35401	347.40	352.7	2	347.26	351.40	351.29	347.25	4.04	0.01163
† Inclusiv	ve Dates:	35405	80 08	19 to 80 11	. 17 (8	calibrating	days) 333	2.29	
		34770	80 09	10 to 80 11	17 (8	calibrating	days) 33	3.84	
		35401	80 08	19 to 80 11	17 (8	calibrating	days) 34	7.40	
*		.		· .					

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Error detected in final proofing of report. Correct value (333.82 ppm) not used in curve fits.

Table 6d. Comparison of the 1980-81 air correction with the 1974 correction. Manometric measurements X are from Table 1a.^{*} The nomenclature is as in Table 6a. The column headed "J81" is obtained by drift correcting the measured J74 in 1974 to the time of the 1981 CO_2 -in-air calibration relative to CO_2 -in-nitrogen standards. The column headed J74X' is obtained by inverting the 1974 calibration curve, CUB1(J), and J81X' results from drift correction of J74X' to the 1981 calibration time.

Measured				Calculated				Points	
Cylinder No.	J74	<u>x</u>	J81X	J74X'	J81X'	J81	ΔJ = J81X'-J81	∆J_/J81 	
35435	330.22	334.11	329.61	334.11	333.43	329.49	3.94	0.01195	
35405	332.86	336.99	332.39	336.88	336.24	332.17	4.07	0.01224	
34770	334.36	338.55	333.88	338.37	337.76	333,69	4.07	0.01219	
35401	347.76	352.96	347.48	351.94	351.51	347.28	4.23	0.01217	
35378	350.26	355.64	349.97	354.42	354.03	349.81	4.22	0.01206	

The adjusted index values, in the column headed 'J74', are from Guenther and Keeling, 1981 p. 70.

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Table 7. Comparison of air and synthetic air CO₂ concentration data (X values in ppm) before and after replacement of the source block trap on October 30, 1980. In the column headed "Before" are summarized comparisons from January 1, 1980 to October 28, 1980. In the column headed "After" are summarized comparisons from October 30 through February 2, 1981. For these six standards, there are manometric measurements in 1974 and 1980.

	Cylinder No.	% 0 ₂	Before	After	After-Before
CO ₂ -in-a	ir Red Strij	pe Cylir	nders		
	35405		336.78±.02	336.91±.02	0.13±.03
	34770	÷	338.37±.02	338.50±.02	0.13±.03
	35401		352.71±.02	352.80±.04	0.09±.04
^{CO} 2-in-n	itrogen and	oxygen	cylinders		
	35452	18.8	323.73±.01	323.83±.02	0.10±.02
	35434	18.8	323.77±.07	323.96±.04	0.19±.08
	35389	20.9	335.12±.06	335.22±.01	0.10±.06#
Wt. Av.	Difference	(in ppm)):		

0.11±.01

#Omitted from average because manometric measurements are almost 0.5 ppm above infrared concentration, indicating that there may be a contaminating gas present. - 27 .

			Date:	6 FEB 81	4 FEB 81	5 FEB 81	4 FEB 81	5 FEB 81
	Cylinder		Pressure(mmHg):	760.46	508.27	255.18	508.27	255.18
	No.	<u>× 0</u> 2	%A		Index I (ppm)	Adjusted	Index J81 (ppm)
^{CO} 2 ⁻	-in-air Red	Stripe ⁺ Cyl	linders					
-	34770	20.95	0.93	329.90	329.20	329.20	333.55	333.00
	35401	20.95	0.93	341.11	340.73	340.20	347.03	346.38
C02-	-in-nitrogen	-and Oxyge	en Standards					
_	127524	100	0.0	319.25	317.83	316.09	319.17	317.05
	127693	100	0.0	334.84	333.41	331.40	338.12	335.68
	75934	79.9	0.0	321.94	320.95	319.49	322.97	321.19
	35442	60.0	0.0	315.10	314.38	313.34	314.97	313.70
	35441	40.2	0.0	322.12	321.66	320.86	323.83	322.86
	35434	18.8	0.0	318.83	318.53	318.25	320.02	319.68

Table 8. Data for pressure correction to air correction.

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Cylinder No.	J (ppm)	∆J (ppm)	∆P (mmHg)	<u>% 0</u> 2	<u>%A</u>	∆J FIT (ppm)	ΔJ-ΔJ FIT (ppm)
	•		н.	. =			
34770	333.55	0.30	252.19	20.95	0.93	0.36	-0.06
35401	347.03	0.46	**	20.95	0.93	0.37	0.09
127524	319.17	1.73	11	100.00	0.0	1.63	0.10
127693	338.12	1.74	11	100.00	0.0	1.73	0.01
75934	322.97	1.20	¥1	79.9	0.0	1.30	-0.10
35442	314.97	0.88	Ħ	60.0	0.0	0.94	-0.06
35441	323.83	0.56	89	40.2	0.0	0.63	-0.07
35434	320.02	0.37	11	18.8	0.0	0.29	0.08
34770	333.00	0.85	505.28	20.95	0.93	0.86	-0.01
35401	346.38	1.11	11	20.95	0.93	0.89	0.22
127524	317.05	3.85	11	100.00	0.0	3.87	-0.02
127693	335.68	4.18	81	100.00	0.0	4.10	0.08
75934	321.19	2.98	T1 .	79.9	0.0	3.09	-0.11
35442	313.70	2.15	H ·	60.0	0.0	2.23	-0.08
35441	322.86	1.53	11	40.2	0.0	1.51	0.02
35434	319.68	0.71	н	18.8	0.0	0.69	0.02

Table 9. Fit of Equation (11) to pressure correction data summarized in Table 8. The column headed " ΔJ " is obtained by subtracting the Index (I) at pressure P (mmHg) from the Index at 760.46 (mmHg) and multiplying it by 1.2186, the ratio $\Delta J/\Delta I$.

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Cylinder No.	SIO Manometric Average Conc. (ppm)	NBS Gravimetric Conc. (ppm)	Difference (ppm)
62206	330.20	333.34	-0.14
61130	339.91	340.05	-0.14
243988	346.68	346.68	0.00

Table 10. Comparisons of Manometric Analyses with NBS Gravimetric Standards

Average Difference (SIO-NBS)

2

< 7

$-0.09 \pm .05$

30 I

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Fig. 1. System drift between 1980 and 1981 calibration periods (see Table 4). The equation for the curve is a quadratic least squares fit and is given in the text as equation (2).

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Fig. 2. Air correction obtained from 1980 and 1981 calibrations. Points are from CO_2 -in-air manometrically analyzed cylinders, compared to Scripps span gases on same day (see Table 6a).



Fig. 3. Comparison of air corrections determined from calibrating data for different periods. The curve and the circled points (\bullet) are for the same data as in Figure 2, and Table 6a. The pluses (+) represent additional comparisons near time of the 1981 CO₂-in-air calibration (Table 6b), the crosses (x) are for CO₂-in-air cylinders compared near the time of the 1980 CO₂-in-nitrogen calibration (Table 6c), and the squares (\bullet) are for the comparisons that lead to the 1974 WMO air correction (Table 6d).

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